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71 Applicant: **IMPERIAL CHEMICAL INDUSTRIES LIMITED**,
Imperial Chemical House Millbank, London SW1P 3JF
(GB)

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72 Inventor: **Backhouse, Alan James, Monks Wood Monks**
Close St. Mary's Hill, South Ascot Berkshire (GB)

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74 Representative: **Wood, Dennis John Cecil et al, Imperial**
Chemical Industries Limited Legal Department: Patents
Thames House North Millbank, London SW1P 4QG (GB)

54 Multi-layer coating process involving use of aqueous basecoat composition containing crosslinked polymer microparticles and having a pseudoplastic or thixotropic character.

57 A process for producing a multi-layer coating upon a substrate surface, in which there is first applied to the surface a pigmented basecoat composition and then there is applied to the basecoat film a transparent topcoat composition; characterised in that the basecoat composition is based upon a dispersion in an aqueous medium of crosslinked polymer microparticles which have a diameter of 0.01-10 microns, are insoluble in the aqueous medium and are stable towards gross flocculation, the dispersion having a pseudoplastic or thixotropic character.

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ACTORUM AG

MULTILAYER COATING PROCESS INVOLVING USE OF AQUEOUS
BASECOAT COMPOSITION CONTAINING CROSSLINKED POLYMER
MICROPARTICLES AND HAVING A PSEUDOPLASTIC OR THIXOTROPIC CHARACTER

This invention relates to the application of protective and decorative coatings to surfaces, particularly the surfaces of automobile bodies..

5 It is well known to employ, especially in the automobile industry, coating compositions which contain metallic pigments; these are the so-called "glamour metallic" finishes whereby a differential light reflection effect, depending on the viewing angle, is achieved. To maximise this "flip" tone effect, careful formulation of
10 the coating composition in regard both to the film-forming resin and to the liquid medium is required. Difficulties may be encountered in formulating a single composition which both meets this objective and at the same time achieves a high degree of gloss in the final
15 finish such as is usually desired in the automobile field. For this reason, one of the procedures which has been proposed for producing metallic finishes is a two-coat procedure, in which there is first applied by spraying, to the surface of the substrate, a basecoat containing
20 the metallic pigment and formulated so as to give the optimum "flip" effect, and there is then applied over the basecoat, again by spraying, an unpigmented topcoat which will yield the desired degree of gloss without in any way modifying the characteristics of the basecoat.

25 For a successful two-coat metallic finish system of this "basecoat/clearcoat" type, an essential criterion is that the basecoat film must be able to resist attack by the solvents in the clearcoat composition when the latter is subsequently applied, in order to avoid disturbance of the metallic pigment and hence impairment of the
30

"flip" effect; it is, moreover, very desirable that the basecoat film should possess this property without the need for an extended intermediate drying or curing operation.

5 In the known basecoat/clearcoat systems, in which both the basecoat and the clearcoat compositions are organic solvent-borne, this requirement has in most cases been met by the use of an additive capable of imparting a gel-like character to the freshly formed basecoat film;
10 the additive which has predominantly been used is cellulose acetate butyrate. The transition between the relatively low viscosity, which the basecoat composition is required to have at the spray gun, and this gel-like character is assisted by arranging that the liquid diluent
15 of the composition contains volatile components which are preferentially lost by evaporation during the passage from the spray gun to the substrate.

 For reasons of avoiding atmospheric pollution, considerable interest has developed in recent years in
20 coating compositions which employ water as the diluent rather than organic solvents. A number of such compositions has been proposed for use in the automobile industry. It has not, however, hitherto been possible to employ water-borne compositions satisfactorily as the basecoat component of a basecoat/clearcoat system. One of the factors
25 tending to inhibit the successful achievement of such an objective is the extreme difficulty of arranging for controlled selective loss of diluent from the basecoat composition by evaporation between spray gun and substrate, except by means of very expensive regulation of the ambient
30 humidity in the spray area. We have, however, now found that a satisfactory water-borne basecoat composition can

be based upon an aqueous dispersion of a crosslinked polymer microgel.

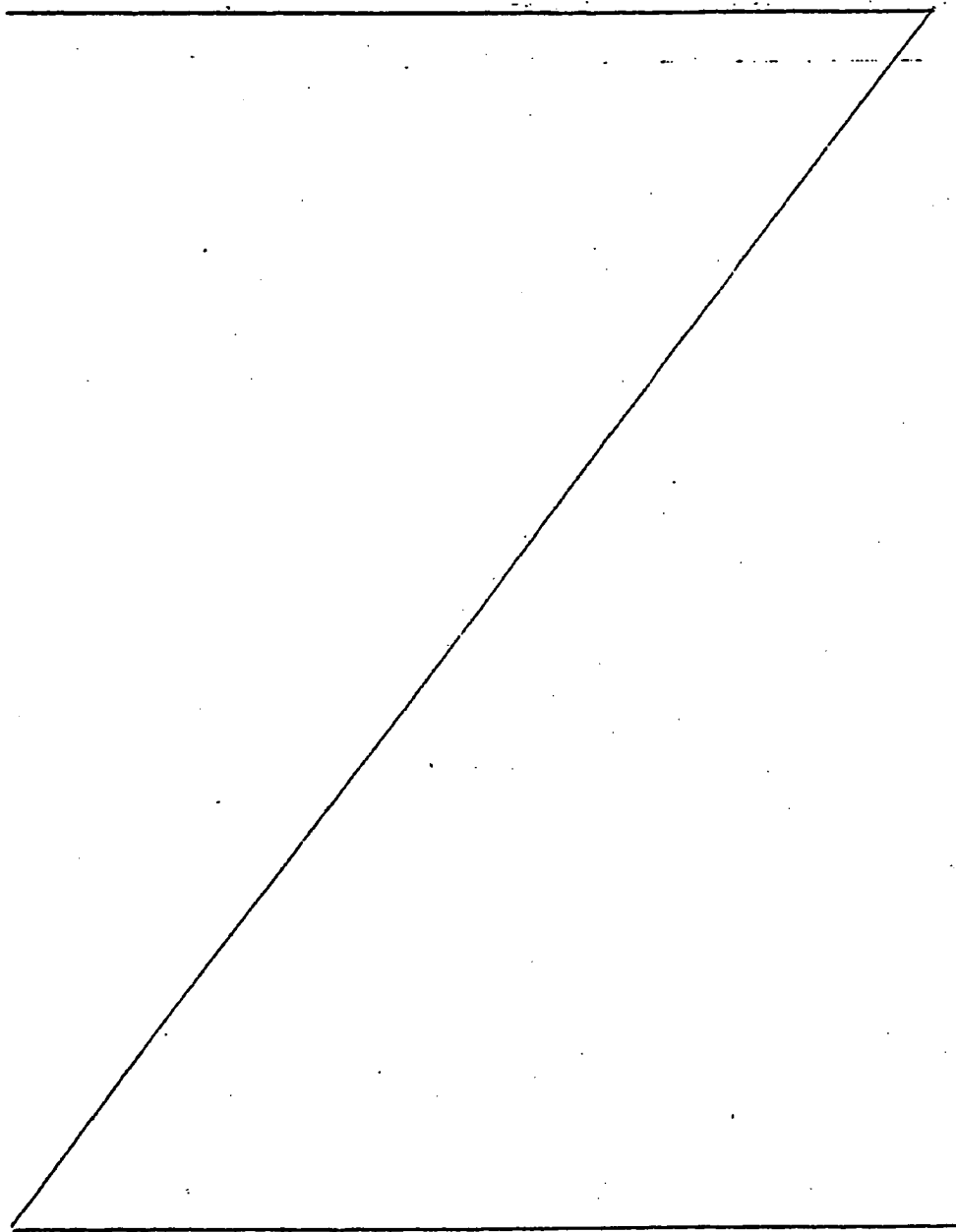
Thus according to the present invention there is provided a process for the production of a multi-layer protective and/or decorative coating upon a substrate surface, which comprises the steps of:-

- (1) applying to the surface a basecoat composition comprising (a) film-forming material (b) a volatile liquid medium for the said material and (c) pigment particles dispersed in the said liquid medium;
- (2) forming a polymer film upon the surface from the composition applied in step (1);
- (3) applying to the basecoat film so obtained a transparent topcoat composition comprising (d) a film-forming polymer and (e) a volatile carrier liquid for the said polymer; and
- (4) forming a second polymer film upon the basecoat film from the composition applied in step (3).

characterised in that the constituents (a) and (b) of the basecoat composition are provided by a dispersion in an aqueous medium of crosslinked polymer microparticles which have a diameter in the range 0.01 to 10 microns, are insoluble in the said aqueous medium and are stable towards gross flocculation, the dispersion having a pseudoplastic or thixotropic character.

The crosslinked polymer microparticles may be composed of various types of polymer. Of particular interest for this purpose are the acrylic addition polymers, derived from one or more alkyl esters of acrylic acid or methacrylic acid, optionally together with other ethylenically unsaturated monomers. Suitable acrylic or methacrylic esters include methyl methacrylate, ethyl methacrylate, propyl methacrylate, butyl methacrylate, ethyl acrylate, butyl

acrylate and 2-ethylhexyl acrylate. Suitable other, copolymerisable monomers include vinyl acetate, vinyl propionate, acrylonitrile, styrene and



vinyl toluene. Since the polymer is required to be cross-linked, there may be included in the monomers from which the polymer is derived a minor proportion of a monomer which is polyfunctional with respect to the polymerisation reaction, e.g. ethylene glycol dimethacrylate, allyl methacrylate or divinylbenzene; alternatively there may be included in those monomers minor proportions of two other monomers carrying pairs of chemical groups which can be caused to react with one another either during or after the polymerisation reaction, such as epoxy and carboxyl (as for example, in glycidyl methacrylate and methacrylic acid), anhydride and hydroxyl or isocyanate and hydroxyl.

The chemical composition and degree of cross-linking of the microparticle polymer may be such that it has a T_g (glass-rubber transition temperature) below room temperature, in which case the microparticles will be rubbery in nature; alternatively, it may be such that the T_g is above room temperature, that is to say the particles will be hard and glassy.

As already specified, it is necessary that the polymer microparticles be dispersed in the basecoat composition in a state which is stable towards gross flocculation, that is to say, a state in which, even at low solids contents, the dispersion contains few if any multi-particle aggregates; this does not, however, preclude the possibility of a slight degree of particle flocculation especially at higher solids contents. This state may be achieved, for example, by steric stabilisation, that is to say by the provision around the particles of a barrier of chains of a different polymer which are solvated by the aqueous medium of the composition

and hence exist in a chain-extended configuration. In this context, the term "solvated" implies that the polymer chains in question, if they were independent molecules, would be actually soluble in the said aqueous medium;

5 however, because the chains are in fact attached to the microparticles at one or more points along their length, the steric barrier remains permanently attached to the microparticles. Polymer microparticles which are sterically stabilised in this way may conveniently be produced by a

10 process of dispersion polymerisation of the appropriate monomers in the aqueous medium, in the presence of a steric stabiliser. The stabiliser is amphipathic in nature, that is to say it contains in the molecule two essential polymeric components of differing characteristics : one

15 component is a polymer chain which is solvated by the aqueous medium, and the other component is a polymer chain which is not solvated by that medium and in consequence anchors itself to the polymer microparticles which are by definition insoluble in the aqueous medium. Suitable dispersion polymerisation processes are described in our

20 British Patent Application No. 7940088 (now published as Application No. 2039497 A). The aqueous medium in which the polymerisation is carried out consists of water admixed with a volatile organic co-solvent, the mixture

25 as a whole being capable of dissolving the monomers, most or all of which would be substantially insoluble in water alone. These procedures involve the additional requirement that the polymerisation be conducted at a temperature which is at least 10°C higher than the glass

30 transition temperature of the polymer which is to be formed, and in such a manner that at no time is there present a separate monomer phase. The amphipathic steric stabiliser may be added to the polymerisation mixture as

a pre-formed substance, or it may be formed in situ during the polymerisation from a polymer which is soluble in the aqueous medium and is able to copolymerise with, or, through hydrogen abstraction, to undergo grafting by, some of the monomer being polymerised. The sterically stabilised microparticle dispersions which are obtained by these procedures are very suitable for the formulation of basecoat compositions to be used in accordance with the present invention, since it is possible to remove the organic co-solvent from them by distillation without impairing the stability of the disperse phase, yielding a product in which the continuous phase consists solely of water.

Alternatively, the dispersion of polymer microparticles may be obtained by the aqueous emulsion polymerisation of the appropriate monomers, in which case the stability towards flocculation is conferred by the presence on the particles of electrically charged species derived from a water-soluble, ionised surfactant and/or a water-soluble, ionisable polymerisation initiator. Such polymerisation processes are extensively described in the literature.

Yet again, the polymer microparticles may be made by a process of non-aqueous dispersion polymerisation of monomers, followed by transfer of the resulting polymer to the aqueous medium. Such a procedure is described in our British Patent Application No. 42457/77. (now published as Application No. 2006229 A). It involves in a first step forming a sterically stabilised dispersion in a non-aqueous liquid of a polymer which is insoluble both in the non-aqueous liquid and in water, using any of the procedures which are well known in the art for making such dispersions; then in a

second step polymerising in the dispersion thus obtained, in the presence of a steric stabiliser, one or more monomers which can give rise to a second polymer which is inherently soluble in the desired aqueous medium at an appropriate pH; and finally transferring the resulting composite polymer microparticles from the non-aqueous medium to the aqueous medium.

The foregoing discussion has centred on the case where the crosslinked polymer microparticles are composed of an addition polymer, this being the most convenient type of polymer for the present purpose. It is possible, however, for the microparticles alternatively to be composed of a condensation polymer, for example a polyester prepared from a polyhydric alcohol and a polycarboxylic acid. Suitable polyhydric alcohols include ethylene glycol, propylene glycol, butylene glycol, 1:6-hexylene glycol, neopentyl glycol, diethylene glycol, triethylene glycol, tetraethylene glycol, glycerol, trimethylolpropane, trimethylolethane, pentaerythritol, dipentaerythritol, tripentaerythritol, hexanetriol, oligomers of styrene and allyl alcohol (for example that sold by Monsanto Chemical Company under the designation RJ 100), the condensation products of trimethylolpropane with ethylene oxide or propylene oxide (such as the products known commercially as "Niax" triols : "Niax" is a Registered Trade Mark). Suitable polycarboxylic acids include succinic acid (or its anhydride), adipic acid, azelaic acid, sebacic acid, maleic acid (or its anhydride), fumaric acid, muconic acid, itaconic acid, phthalic acid, (or its anhydride), isophthalic acid, terephthalic acid, trimellitic acid (or its anhydride) and pyromellitic acid (or its anhydride). Such polymers are caused to be crosslinked by the incorporation of materials of function-

ality greater than two in the starting composition,
although in this case, because of the characteristically
broad distribution of molecular species formed in a
condensation polymerisation as compared with that of an
5 addition polymerisation, it may be difficult to ensure
that all these species are in fact crosslinked.

It will be appreciated that the methods which
have been referred to above for making polymer micro-
particles by polymerisation of addition-type monomers in
10 an aqueous medium are not, in general, applicable to
condensation-type monomers because of the inhibiting
effect of water on the condensation reaction. Condensation
polymer microparticles may, however, readily be made by
dispersion polymerisation in non-aqueous media according
15 to the procedures described in our British Patent Specif-
ications Nos. 1,373,531; 1,403,794 and 1,419,199 and
methods of obtaining crosslinked microparticles are
included in these descriptions. Such microparticles may
then be subjected, in dispersion in the non-aqueous
20 medium, to the second polymerisation step of the procedure
of British Patent Application No. 42457/77 (published
Application No. 2006229A) referred to above, followed by
their transfer to the chosen aqueous medium.

By "aqueous medium" is meant herein either
25 water alone or water in admixture with a water-miscible
organic liquid such as methanol; the aqueous medium may
also contain water-soluble substances introduced for the
purpose of adjusting the pH of the basecoat composition
as discussed in more detail below.

30 The pigment particles which, as already defined,
are dispersed in the aqueous medium of the basecoat comp-

osition may range in size from 1 to 50 microns and may be of any of the pigments conventionally used in surface coating compositions, including inorganic pigments such as titanium dioxide, iron oxide, chromium oxide, lead chromate and carbon black, and organic pigments such as phthalocyanine blue and phthalocyanine green, carbazole violet, anthrapyrimidine yellow, flavanthrone yellow, isoindoline yellow, indanthrone blue, quinacridone violet and perylene reds. For the present purposes, the term "pigment" is here meant to embrace also conventional fillers and extenders, such as talc or kaolin.

The process of the invention is of particular relevance to the case of basecoat compositions containing metallic flake pigmentation which are intended for the production of "glamour metallic" finishes chiefly upon the surfaces of automobile bodies as previously discussed, suitable metallic pigments including in particular aluminium flake and copper bronze flake. However, the invention offers advantages also in the production of "solid colour" finishes, as discussed below. In general, pigments of any kind may be incorporated in the basecoat compositions in an amount of from 2% to 100% of the total weight of the composition. Where metallic pigmentation is employed, this is preferably in an amount of from 5% to 30% by weight of the aforesaid total weight.

Such pigments, whether metallic or otherwise, may be incorporated into the basecoat compositions with the aid of known pigment dispersants suitable for use in aqueous systems.

The presence of the crosslinked polymer micro-particles in the basecoat composition confers upon the film derived from the latter the desired ability to withstand subsequent application of the topcoat composition

without disturbance of the film or of the pigmentation, in particular metallic pigmentation, which it contains and without which, therefore, a successful basecoat/clear-coat system cannot be achieved.

5 In addition to this essential feature, it is also required, as stated above, that the dispersion of insoluble microparticles should possess a pseudoplastic or thixotropic character. By this is meant that the apparent viscosity of the dispersion will differ according to the degree of shear to which the dispersion is subjected and, more particularly, that the apparent viscosity under low shear is greater than it is under high shear. The change in viscosity consequent upon a change in the shear applied may be instantaneous or it may require a finite time interval which is nevertheless within the time scale of the viscosity measurement. The reason for requiring this character in the dispersion on which the basecoat composition is based is most apparent in the case where that composition contains a metallic flake pigment. It is then desirable that the total concentration of non-volatile solids present should be relatively low, in order to achieve a substantial shrinkage of the basecoat film after application to the substrate and during the drying operation, and thereby to ensure correct orientation of the metallic flake and hence optimum "flip" effect. It is, however, necessary, where the basecoat composition is to be applied to a substrate by spraying, that the composition should have a low enough viscosity for efficient atomisation at the spray gun, and yet, once it has reached the substrate, that its viscosity should be high enough to prevent "sagging" or "running" of the film, or the development of "sheariness" (uneven distribution and orientation) of the metallic flake, even if the loss of water and other

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solvents by evaporation between the spray gun and the substrate is only slight (owing to a high ambient humidity).

The possession of such pseudoplastic properties is often expressed by quoting values of η_a (apparent viscosity in poise) at selected values of D (shear rate in sec^{-1}). In the case of metallic pigmented basecoat compositions to be used according to the invention, the value of η_a , at a solids content of less than 30% by weight non-volatiles, should preferably be less than 0.5 poise at a shear rate D of $10,000 \text{ sec}^{-1}$, and more than 20 poise at a value of D of 1.0 sec^{-1} . Even more preferably, the basecoat composition should have a value of η_a of less than 0.25 poise at a value of D of $10,000 \text{ sec}^{-1}$ and of more than 40 poise at a value of D of 1.0 sec^{-1} . In the case of "solid colour" basecoat compositions incorporating pigments other than metallic flake, it is preferred that η_a , again at solids contents below 30%, should be less than 1 poise at $D = 10,000 \text{ sec}^{-1}$ and more than 5 poise at $D = 1.0 \text{ sec}^{-1}$; even more preferably, η_a is less than 0.7 poise at $D = 10,000 \text{ sec}^{-1}$ and more than 10 poise at $D = 1.0 \text{ sec}^{-1}$. It is, however, in the nature of pseudoplastic or thixotropic behaviour that it cannot be fully and accurately defined by a few selected viscosity/shear data; much depends upon the actual method of viscosity measurement employed. It is, therefore, not intended that the values quoted above should be considered as rigid limits which must be adhered to in order to achieve the benefits of the invention; they are, rather, given as an approximate guide only and the skilled person can readily determine, by simple practical tests, whether a particular dispersion, or the basecoat composition derived from it, possesses the necessary degree of pseudo-

plasticity or thixotropy.

There are various ways in which a pseudoplastic or thixotropic character can be conferred upon the base-coat dispersion. In certain cases, no special measures are required. This may be so, for example, where the microparticles have been prepared by the above-mentioned procedure described in British Patent Application No. 42457/77 (published Application No. 2006229A). This procedure involves first of all the production of the polymer microparticles proper by a process of non-aqueous dispersion polymerisation of the appropriate monomers, followed by polymerisation of further monomers in order to produce a second polymer which is essentially non-crosslinked and is of a hydrophilic character such that it is inherently capable of dissolving in the aqueous medium in which the final dispersion is to be formed, at an appropriate pH. Not all this second polymer does, however, in fact dissolve in the aqueous medium on the transferring to it of the product of these two non-aqueous polymerisation steps. A substantial part of the second polymer remains associated with the polymer microparticles, and the microparticles are thereby stabilised in dispersion in the aqueous medium; at the same time, however, this associated polymer may result in the aqueous dispersion exhibiting pseudoplastic or thixotropic properties. Further monomers which are suitable for use in the second polymerisation step are, for example, a hydroxyalkyl ester of acrylic acid or methacrylic acid, a monoacrylic or monomethacrylic ester of a polyglycol such as polyethylene glycol, a monovinyl ether of such a polyglycol, or vinyl pyrrolidone, optionally in admixture with smaller proportions of non-hydrophilic monomers such as methyl methacrylate, butyl acrylate, vinyl acetate or styrene.

Alternatively, or additionally, the required solubility in the aqueous medium can be achieved by using as a major monomer constituent an acrylic ester containing basic groups, for example dimethylaminoethyl methacrylate or diethylaminoethyl methacrylate, these groups being subsequently converted to salt groups by reaction with a suitable acid, for example lactic acid, dissolved in the aqueous medium. Yet again, the second polymer may be derived from comonomers containing a substantial proportion of a polymerisable carboxylic acid, such as acrylic acid or methacrylic acid, and is then capable of dissolving in an aqueous medium containing a dissolved base, such as dimethylaminoethanol. In general, therefore, the second polymer may be non-ionic, anionic or cationic in character.

Where the polymer microparticles have been made by a process of aqueous emulsion polymerisation as is well known in the art, a second, inherently water-soluble, polymer may be produced by further polymerisation, in the same aqueous medium and in the presence of the microparticles, of monomers giving rise to a polymer which contains acidic salt-forming groups that can confer water-solubility. Thus suitable monomers are polymerisable carboxylic acids such as acrylic acid or methacrylic acid, if desired together with minor proportions of non-hydrophilic monomers such as methyl methacrylate and also of hydrophilic monomers which give rise to water-insoluble homopolymers, e.g. hydroxyethyl methacrylate and hydroxypropyl methacrylate.

Where the polymer microparticles have been made by a process of dispersion polymerisation in an aqueous medium as described above with reference to our British Patent Application No. 7940088 (published Application No.

2039497A), the second, water-soluble polymer can conveniently be generated by further polymerisation in the same medium of suitable monomers such as those mentioned in the preceding paragraph and also basic monomers such as dimethylaminoethyl methacrylate, from which water-soluble salt derivatives can be generated.

Not all water-soluble polymers generated in situ in the presence of the microparticles by any of the above-described methods will be capable of conferring the desired pseudoplastic properties upon the basecoat composition, but suitable polymer compositions can be arrived at by a process of simple trial experimentation involving, for example, measurements of viscosity at selected different shear rates as described above, or actual application of the compositions to a substrate.

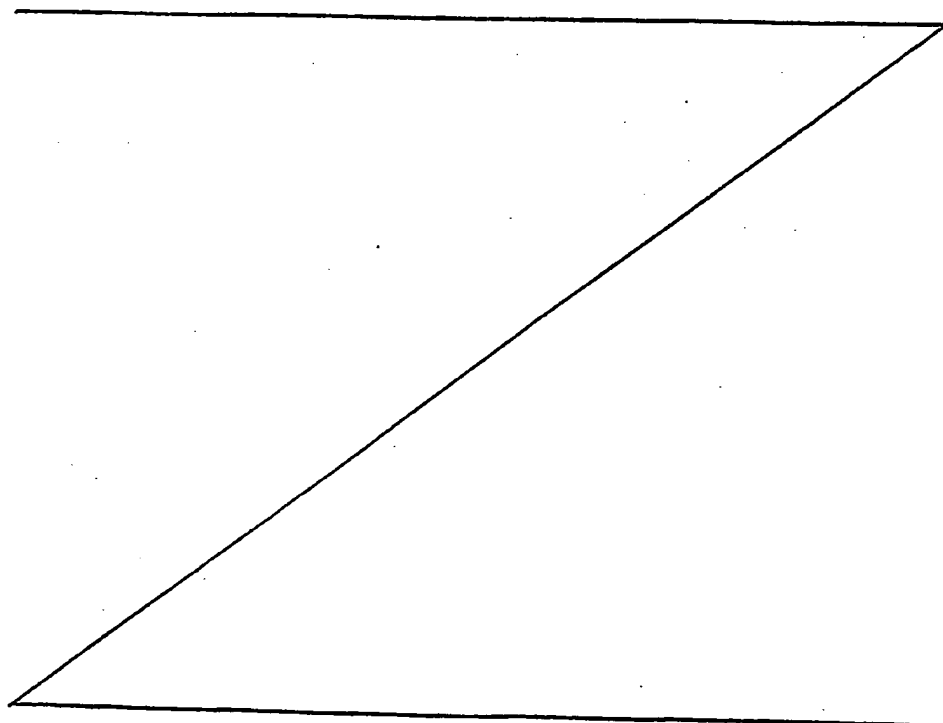
Instead of generating a suitable water-soluble polymer in situ, or in addition thereto, such a polymer may be added, as a pre-formed separate ingredient, to the aqueous dispersion of the microparticles. Suitable polymers are those which, when dissolved in the aqueous medium even at low concentrations, bring about a considerable enhancement of the viscosity of the composition. For example, there may be added one or more of the thickeners which are well known for use in coating compositions based on aqueous polymer latices. Not all such thickeners are, however, suitable for the present purpose, since some thickeners are not capable of conferring the necessary pseudoplastic properties upon the composition to which they are added. On the other hand, certain thickeners which when alone dissolved in the aqueous medium do not exhibit such properties may confer those properties upon the dispersion of the microparticles through interactions between it and the microparticles (e.g. through hydrogen

bonding or interaction of polar groups). One commercially available thickener which has been found to be very suitable is "Acrysol" ASE60, made by Rohm & Haas ("Acrysol" is a Registered Trade Mark).

5 Whilst it follows that any inherently water-soluble polymer which is associated with the polymer microparticles or is added to the microparticle dispersion, for the purpose of imparting pseudoplastic or thixotropic properties to the dispersion, must of its nature be non-
10 crosslinked, such polymer may nevertheless if desired, be of the crosslinkable type. That is to say, it may contain chemically reactive groups whereby it may be caused, optionally with the aid of an added crosslinking agent, to become crosslinked after application of the basecoat
15 composition, and preferably also of the topcoat composition, to the substrate. Thus the polymer may contain, as already indicated, hydroxyl or carboxyl groups derived from monomers bearing those groups, and may be subsequently cross-linked with the aid of an amino resin, e.g. a methylated
20 melamine-formaldehyde condensate, which is soluble in the aqueous medium.

 From the foregoing description, it will be seen that the basecoat composition can consist exclusively of the polymer microparticles, the pigment particles, the
25 aqueous medium in which both groups of particles are dispersed, and inherently water-soluble polymer which imparts pseudoplastic properties to it. However, it is much preferred that the composition should also incorporate a film-forming polymer which is soluble in the aqueous medium, in
30 order to ensure that, subsequent to the application of the basecoat to a substrate and evaporation of the aqueous medium, there is material present which can coalesce so as to fill the voids between the microparticles and thus

produce a coherent, adequately integrated film in step (2) of the process. This function may indeed be fulfilled by a portion of an inherently water-soluble polymer which is present in the composition, as described above, for the purpose of conferring pseudoplastic or thixotropic properties upon it, but, in view of the generally low proportions of such polymer which is required for that purpose, it may be desirable to supplement it by one or more other water-soluble film-forming materials introduced into the composition, which may optionally be chemically reactive with constituents already present. Thus the composition may contain oligomeric substances which can be converted to high molecular weight products subsequent to application of the composition but which do not in themselves contribute significantly to the viscosity of the composition before application.



In this connection there may be mentioned diols of low volatility such as 2-ethyl-1, 3-hexanediol, low molecular weight polypropylene glycols, low molecular weight adducts of ethylene oxide with dihydric or trihydric

5 alcohols such as neopentyl glycol, bisphenol A, cyclohexanedimethanol, glycerol and trimethylolpropane, β -hydroxyalkylamides such as N,N,N¹,N¹- tetrakis - (β -hydroxyethyl) adipamide and cyclic amides and esters such as ϵ -caprolactam and ϵ -caprolactone. Where such

10 materials are not significantly soluble in pure water, they should be soluble in the aqueous medium consisting of water together with the water-miscible organic liquid as previously described. Any of these oligomeric substances can be converted to a high molecular weight

15 polymer, after application of the basecoat composition to the substrate, by linking them through their hydroxyl or other reactive groups by means of a polyfunctional reactant also present in the composition. Particularly useful for this purpose are amino resins soluble in the

20 aqueous medium of the composition, in particular melamine-formaldehyde condensates such as hexa(alkoxymethyl) melamines and their low molecular weight condensates.

As an alternative to its containing constituents which produce a film-forming polymer subsequently to its

25 application to the substrate, the basecoat composition may contain a pre-formed water-soluble acrylic polymer which does not confer pseudoplastic properties upon it, or it may contain in dispersion particles of non-cross-linked polymer which are stabilised in a similar fashion

30 to the crosslinked microparticles present. Either of such alternative constituents may, if desired, contain functional groups such as hydroxyl groups whereby they can

become crosslinked, after application of the composition to the substrate, by means of a crosslinking agent, e.g. an amino resin.

The relative proportions of the various constituents of the basecoat composition may vary widely and the optimum proportions in any individual system are often best determined by experiment, but some generally guiding principles can be stated. In particular, if the proportion of the polymer microparticles is too high in relation to the other film-forming material present in the composition, as described above, there will not be sufficient of the latter material to fill the voids between the microparticles; in consequence, on subsequent application of the clearcoat composition there will be a tendency for that composition to sink into the basecoat film, with resultant loss of gloss. If, on the other hand, the proportion of microparticles is too low, it may not confer on the basecoat composition the desired degree of protection against attack by the solvent present in the clearcoat composition; to some extent, a lower level of microparticles can be compensated for in this respect by allowing a longer period for the basecoat film to flash off or dry off before the clearcoat is applied, but this diminishes one of the chief advantages to be gained from the present invention. In general, a satisfactory level of the microparticles will lie in the range 5 - 80% by weight of the total non-volatile content of the basecoat composition. The optimum level depends, however, in some degree upon whether the pigment present in the basecoat composition is metallic or non-metallic. For "metallic" compositions, the preferred range of microparticle content is 40-75% by weight on the foregoing basis. For "solid colour" compositions, because of the generally higher

proportions of pigment required in order to achieve adequate opacity at fairly low film thicknesses, the preferred microparticle content range is rather lower, namely 10 - 50% by weight on the same basis as before. The
5 reduced proportion of microparticles avoids an excessively high total volume fraction of dispersed material which could result in a porous basecoat film and hence sinkage into it, and poor gloss, of the topcoat film.

Again in general terms, it may be stated that
10 the proportions used in the composition of a thickener, or of a second polymer conferring pseudoplastic properties, may range from 0.3% to 50% by weight of the total non-volatile content; the amount present of other film-forming material may be in the range 0 - 30% by weight and, where
15 a cross-linking agent such as an amino-resin is present, this also may amount to up to 30% by weight of the total non-volatile content of the basecoat composition. The basecoat composition may, if desired, additionally contain a catalyst for any crosslinking reaction which is required
20 to take place after application of the composition to the substrate. This may be a water-soluble acidic compound, such as p-toluenesulphonic acid, orthophosphoric acid, maleic acid or other strong carboxylic acid such as tetrachlorophthalic acid; alternatively, it may be a heat-labile
25 salt of such an acid with a volatile amine.

The nature of the film-forming polymer constituent of the topcoat composition employed in step (3) of the process of the invention is in no way critical. There may in general be used any suitable film-forming polymer,
30 which may be of either the thermosetting or the thermoplastic type. One suitable class of polymer consists of those which are derived from one or more ethylenically unsaturated monomers. Particularly useful members of this

class are the acrylic addition polymers which are well-established for the production of coatings in the automobile industry, that is to say polymers or copolymers of one or more alkyl esters of acrylic acid or methacrylic acid, optionally together with other ethylenically unsaturated monomers. Suitable acrylic esters include methyl methacrylate, ethyl methacrylate, propyl methacrylate, butyl methacrylate, ethyl acrylate, butyl acrylate and 2-ethylhexyl acrylate. Suitable other, copolymerisable monomers include vinyl acetate, vinyl propionate, acrylonitrile, styrene and vinyl toluene. Where the acrylic polymer is required to be of the thermosetting crosslinking type, suitable functional monomers to be used in addition to the latter include acrylic acid, hydroxyethyl acrylate, hydroxyethyl methacrylate, 2-hydroxypropyl acrylate, 2-hydroxypropyl methacrylate, N-(alkoxymethyl) acrylamides and N-(alkoxymethyl) methacrylamides, where the alkoxy groups may be, for example, a butoxy group, glycidyl acrylate and glycidyl methacrylate. The topcoat composition may in such a case contain also a crosslinking agent such as a diisocyanate, a diepoxide or, especially, a nitrogen resin, that is to say, a condensate of formaldehyde with a nitrogenous compound such as urea, thiourea, melamine or benzoguanamine, or a lower alkyl ether of such a condensate in which the alkyl group contains from 1 to 4 carbon atoms. Particularly suitable crosslinking agents are melamine-formaldehyde condensates in which a substantial proportion of the methylol groups have been etherified by reaction with butanol.

The topcoat composition may incorporate a suitable catalyst for the crosslinking reaction between the acrylic polymer and the crosslinking agent, for example an acid-reacting compound such as acid butyl maleate, acid butyl phosphate or p-toluene sulphonic acid. Alternatively the catalytic action may be supplied by the incorporation of free acid groups in the acrylic polymer, for example by the use of acrylic acid or methacrylic acid as comonomer in the preparation of the polymer.

The topcoat polymer may be either in solution or in stable dispersion in the volatile carrier liquid of the topcoat composition, in other words, the carrier liquid may be either a solvent or a non-solvent for the topcoat polymer. Where the liquid is to be a solvent, it may be any of the organic liquids, or mixtures of organic liquids, which are conveniently used as polymer solvents in coating compositions, for example aliphatic hydrocarbons such as hexane and heptane, aromatic hydrocarbons such as toluene and xylene, and petroleum fractions of various boiling point ranges which are predominantly aliphatic but have a significant aromatic content, esters such as butyl acetate, ethylene glycol diacetate and 2-ethoxyethyl acetate, ketones such as acetone and methyl isobutyl ketone, and alcohols such as butyl alcohol. The actual liquid or mixture of liquids selected as the carrier liquid will depend upon the nature of the topcoat polymer, according to principles which are well-known in the coatings art, in order that the polymer shall be soluble in the liquid.

Where the carrier liquid is to be an organic non-solvent, it will tend to be of rather lower polarity than those just mentioned and may consist of one or more aliphatic hydrocarbons such as hexane, heptane or

5 petroleum fractions of low aromatic content, optionally in admixture with liquids of high polarity such as have already been referred to, provided that the total mixture is a non-solvent for the topcoat polymer. In such a case, the topcoat composition will be a non-aqueous polymer

10 dispersion, and this will in general be a sterically stabilised dispersion in which the polymer particles are stabilised by means of a block or graft copolymer, one polymeric constituent of which is non-solvatable by that liquid and is associated with the disperse polymer. The

15 well-known principles according to which such dispersions may be prepared have been extensively described in the patent and other literature, for example in British Patent Specifications Nos. 941,305; 1,052,241; 1,122,397; and 1,231,614 and in "Dispersion Polymerisation in

20 Organic Media" ed. K.E.J.Barrett (John Wiley and Sons, 1975).

Alternatively the topcoat composition may, like the basecoat composition, be water-borne and in this case also the topcoat polymer may be either in solution or in

25 a state of stable dispersion in an aqueous medium. In the case of a dispersion, this may be sterically stabilised, as for example when it has been prepared by an aqueous dispersion polymerisation procedure such as that of British Patent Application No. 7940088 (published Appli-

30 cation No. 2039497A) already referred to, or charge-stabilised, as for example when it has been prepared by the well known aqueous emulsion polymerisation techniques.

Unlike the polymer microparticles of the basecoat composition, the topcoat polymer will always be of the thermosetting type and hence capable of becoming cross-linked after application to the substrate, optionally
5 with the aid of a crosslinking agent.

Usually, the topcoat composition will be substantially colourless so that the pigmentation effect due to the basecoat is not significantly modified, but it may be desirable in some cases, more usually where the
10 basecoat contains a metallic pigment, to provide a transparent tinting of the topcoat composition.

In the first operational step of the process of the invention, the basecoat composition is applied to the surface of the substrate, which may be previously primed
15 or otherwise treated as conventional in the art. The substrates which are of principal interest in the context of the invention are metals such as steel or aluminium which are commonly used for the fabrication of automobile bodies, but other materials such as glass, ceramics, wood
20 and even plastics can be used provided they are capable of withstanding the temperatures at which final curing of the multilayer coating may be effected. After application of the basecoat composition, a polymer film is formed therefrom upon the surface of the substrate. If desired,
25 this may be achieved by subjecting the substrate and the applied coating to heat in order to volatilise the water and any organic liquid diluent therein, and it lies within the scope of the invention to employ a heating temperature sufficient to crosslink the basecoat film in those cases
30 where the composition contains a film-forming material of the thermosetting type. However, a particular merit of the present invention is that it is sufficient to allow

only a short period of drying in order to ensure that the topcoat composition can be applied to the basecoat film without there being any tendency for the former to mix with or dissolve the latter in a way which can, for example, interfere with the correct orientation of metallic pigmentation, whereby optimum "flip" effect is achieved. Suitable drying conditions in any individual case will depend, inter alia, on the ambient humidity but in general a drying time of from 1 to 5 minutes at a temperature of from 15° to 80°C will be adequate to ensure that mixing of the two coats is prevented. At the same time, the basecoat film is adequately wetted by the topcoat composition, so that satisfactory inter-coat adhesion is obtained.

After application of the topcoat composition to the basecoat film, the coated substrate may be subjected to a heating or curing operation in which the volatile carrier liquid of the topcoat is driven off and optionally in which the film-forming material of the topcoat and/or that of the basecoat, is crosslinked with the aid of the crosslinking agent(s) present. This heating or curing operation is usually carried out at a temperature in the range 100 - 140°C, but, if desired, a lower temperature than this may be employed provided it is sufficient to activate any necessary crosslinking mechanism.

In performing the process of the invention, the basecoat and topcoat compositions may be applied to the substrate by any of the conventional techniques such as brushing, spraying, dipping or flowing, but it is preferred that spray application be used since the best results are thereby achieved in regard to both pigment

control, especially of metallic pigment orientation, and gloss. Any of the known spray procedures may be adopted, such as compressed air spraying, electrostatic spraying, hot spraying and airless spraying, and either manual or
5 automatic methods are suitable.

The thickness of the basecoat-film applied is preferably from 0.5 to 1.5 mils and that of the topcoat from 1 to 3 mils (dry film thickness in each case).

As will be apparent from the foregoing description, the advantage of the invention, so far as "glamour metallic" finishes are concerned, is the provision of a
10 basecoat/clearcoat system in which atmospheric pollution drawbacks are eliminated or much reduced by the use of a water-borne basecoat composition, without the sacrificing of good control of the orientation of the metallic pigment-
15 ation. Where "solid colour" finishes are concerned, control of the orientation of the pigment is, of course, no longer a significant factor, but it remains an advantage that the basecoat film is not disturbed by the
20 subsequent application of the topcoat composition and it is also found that the basecoat film is much less subject to the effect known as "popping" than is a water-borne coating which does not contain the polymer microparticles.

The invention is illustrated but not limited by
25 the following Examples, in which parts and percentages are by weight. In these Examples, the quoted apparent viscosity values η_a of basecoat compositions were determined using two different instruments. The values of η_a at 10,000 sec⁻¹ shear rate were measured using the ICI
30 Cone and Plate Viscometer in the modification designed to cover the viscosity range 0 - 2.0 poise at the shear rate in question. This instrument is described in Journal of

the Oil and Colour Chemists' Association, July, 1966, in an article by C.H. Monk and is manufactured by Research Equipment (London) Limited.

5 The values of η_a at 1.0 sec^{-1} shear rate were measured using a "Rheomat 30" concentric cylinder viscometer with the 'A' cup and bob; each sample was subjected to an applied shear rate of 660 sec^{-1} until a constant shear stress reading was obtained, after which the shear rate was immediately changed to 1.0 sec^{-1} ,
10 the shear stress measured and the viscosity calculated from these data. The "Rheomat 30" is manufactured by Contraves AG of Zurich; "Rheomat" is a Registered Trade Mark.

EXAMPLE 1

15 A. Preparation of dispersion of polymeric micro-particles in aliphatic hydrocarbon.

To a reactor fitted with stirrer, thermometer, reflux condenser and provision for adding monomer to the returning distillate was charged 35.429 parts of heptane.
20 The latter was heated to reflux temperature ($95 - 96^\circ\text{C}$) and the following premixed ingredients were then added:-

Methyl methacrylate	5.425 parts
Azodiisobutyronitrile	0.420 part
Graft copolymer stabiliser (33% solution as described below)	1.984 parts

25 The contents of the reactor were held at reflux temperature for 30 minutes so as to form a "seed" dispersion of polymer, after which the following premixed ingredients were fed into the returning distillate at a steady rate over a period of 3 hours:-

30

methyl methacrylate	25.000 parts
allyl methacrylate	0.775 part
azodiisobutyronitrile	0.338 part
graft copolymer stabiliser (33% solution as described below)	5.316 parts

5 After completion of the feed, the contents of
the reactor were held at reflux temperature for a further
1 hour, following which 12.874 parts of heptane was added
and refluxing resumed. The following premixed ingredients
were fed into the reactor via the returning distillate at
10 a steady rate over 1 hour:-

methyl methacrylate	3.883 parts
butyl acrylate	3.066 parts
hydroxyethylacrylate	2.044 parts
acrylic acid	1.226 parts
15 azodiisobutyronitrile	0.071 part
graft copolymer stabiliser (33% solution as described below)	2.149 parts

Following completion of this feed, the reaction
mixture was held at reflux temperature for 1 hour. A
stable dispersion of crosslinked polymer microparticles
20 was obtained having a total non-volatile solids content
of 43.5 - 44.5% and a content of non-volatile solids
insoluble in any polar solvent (viz. gel content) of
34.5 - 35%.

The graft copolymer stabiliser used in the
25 above procedure was obtained as follows. 12-Hydroxy-
stearic acid was self-condensed to an acid value of
about 31 - 34 mg KOH/g (corresponding to a molecular
weight of 1650 - 1800) and then reacted with an equival-
ent amount of glycidyl methacrylate. The resulting
30 unsaturated ester was copolymerised at a weight ratio of

2:1 with a mixture of methyl methacrylate and acrylic acid in the proportions of 95:5. The copolymer was used as a 33% solution in a mixture of ethyl acetate 11.60% , toluene 14.44% , aliphatic hydrocarbon b.p. 98 - 122°C 61.29% and aliphatic hydrocarbon b.p. 138 - 165°C 12.67%.

B. Transfer of the polymer microparticles to dispersion in aqueous medium.

To a reactor fitted with stirrer, thermometer and means for removing volatile solvent by distillation was charged:-

demineralised water	72.308 parts
butoxyethanol	10.332 parts
dimethylaminoethanol	0.529 part

The contents of the reactor were heated to 100°C and 46.497 parts of the microparticle dispersion from stage A were then fed in at such a rate that the heptane contained in the dispersion was removed by distillation without building up any significant concentration in the contents of the reactor. The time required to do this was about 2 hours and the distillate, consisting mainly of heptane with some water, amounted to 29 - 30 parts.

The product was a stable aqueous dispersion of the polymer microparticles having a non-volatile solids content of 20 - 22% and a pH of 7.2 - 7.5.

C. Preparation of aluminium pigment concentrate

To a stirred mixing vessel was charged:-

aluminium paste (metal content, 65%)	5.8 parts
butoxyethanol	2.9 parts

These ingredients were stirred together for 15 minutes and a further 2.9 parts of butoxyethanol was then added at a steady rate over 30 minutes, following which the mixture was stirred for a further 1 hour. There was then

added 4.84 parts of hexamethoxym thylmelamine and stirring was continued for 1 hour; finally, a further 1.93 parts of hexamethoxymethylmelamine and 0.97 part of butoxy-ethanol were added and the mixture was stirred for 1 hour

5: more.

D: Preparation of basecoat composition

The following ingredients:-

	aluminium concentrate from stage C	19.34 parts
	microparticle dispersion from stage B	79.61 parts
10	hexamethoxymethylmelamine	0.46 part
	dimethylaminoethanol salt of p-toluenesulphonic acid, 10% solution in demineralised water,	3.57 parts

were stirred together for 1 hour. The basecoat composition thus obtained had the following characteristics:-

	Solids content :	27.2%
15	Apparent viscosity η_a :	35 poise at shear rate D = 1 sec ⁻¹ 0.06 poise approx. at shear rate D = 10,000 sec ⁻¹ .

E. Preparation of acrylic polymer for clearcoat composition.

20 To a reactor fitted with stirrer, thermometer and reflux condenser was charged:-

	xylene	22.260 parts
	aromatic hydrocarbon b.p. 190 - 210°C	10.000 parts

25 The mixture was heated to reflux temperature (142-146°C) and the following premixed ingredients were added at a steady rate over 3 hours:-

	styrene	21.49 parts
	ethyl acrylate	4.51 parts
	2-ethylhexylacrylate	13.75 parts
	hydroxyethyl acrylate	10.05 parts
5	acrylic acid	0.49 parts
	cumene hydroperoxide	1.41 parts

The reactants were held at reflux temperature for a further 2 hours, after which there was added:-

	isobutyl alcohol	12.72 parts
10	xylene	3.32 parts

A clear solution of polymer was thus obtained, having a solids content of 50%.

F. Preparation of solvent-borne clearcoat composition.

15 The following ingredients were blended together:-

	polymer solution from stage E	53.3 parts
	butylated melamine-formaldehyde resin, 67% solution in butanol	26.5 parts
	dipentene	5.0 parts
20	flow-promoting polymer, 10% solution in xylene	0.1 part
	isobutyl alcohol	2.0 parts
	xylene	13.1 parts

A clear solution of 44.4% solids was obtained. It had a viscosity of 40 secs. (B.S. B4 cup at 25°C).

25 G. Application of basecoat and clearcoat to a substrate.

A metal panel was prepared with primer and surfacer, then two coats of the metallic basecoat composition described in stage D were applied by spray, without further thinning, at a temperature of 22°C and a relative humidity of 39%. A two-minute flash-off

30

period was allowed between the coats; the paint flow rate at the spray gun was 400 mls/minute.

5 After application of the second basecoat the panel was blown with air at 25°C and two coats of clearcoat composition as described in stage F were applied, the clearcoat composition having been thinned beforehand with xylene to a viscosity of 45 secs (B.S. B3 cup at 25°C). The two coats were applied wet on wet with a two-minute flash-off period between the coats. After a final 10 three-minute flash-off, the panel was stoved at 125-130°C for 30 minutes.

The resulting silver metallic coating had excellent 'flip' and absence of 'shear', and was equivalent in appearance to finishes of the highest degree of 15 'flip' obtained from a completely solvent-borne paint system. The gloss and intercoat adhesion were good and there was no sinkage of the clearcoat into the basecoat.

EXAMPLE 2

20 A metal panel was prepared with primer and surfacer, then two coats of the metallic basecoat composition described in stage D of Example 1 were applied by spray, without further thinning, at a temperature of 25°C and a relative humidity of 58%. A two-minute flash-off period was allowed between the coats; 25 the paint flow rate at the spray gun was 400 mls/minute.

After application of the second basecoat, the panel was dried at 35-42°C for 10 minutes and there were then applied two coats of the clearcoat composition described in stage F of Example 1, the clearcoat having 30 been thinned beforehand with xylene to a viscosity of

45 seconds (B.S. B3 cup at 25°C). The two coats were applied wet-on-wet with a two-minute flash-off period between the coats. After a final three-minute flash-off, the panel was stoved at 125-130°C for 30 minutes.

5 The coating thus obtained had the same excellent characteristics as that described in Example 1.

EXAMPLE 3

A. Preparation of aqueous dispersion of polymer microparticles.

10 The following premixes were prepared:-

(i) Monomer premix

methyl methacrylate	18.350 parts
allyl methacrylate	1.340 parts
styrene	4.700 parts
15 butyl acrylate	18.800 parts
methacrylic acid	1.410 parts
prim-octyl mercaptan	0.159 part
ammonium salt of sulphate of (nonylphenol + 5 mols. ethylene oxide)	0.185 part

(ii) Initiator solution

20 ammonium persulphate	0.130 part
demineralised water	4.010 parts

(iii) Surfactant solution

methyl methacrylate	20.000 parts
ammonium salt of sulphate of (nonylphenol + 5 mols. ethylene oxide)	20.000 parts

25 To a reactor, fitted with stirrer, thermometer, reflux condenser and means for controlled introduction of two separate liquid feeds, was charged:-

demineralised water	47.641 parts
surfactant solution (iii)	0.100 part

The charge was heated to 80-85°C, then 2.000 parts of monomer premix (i) were added and the mixture held at 80-85°C for 15 minutes. There was then added 1.068 parts of initiator solution (ii) and the reaction mixture was held at the same temperature for 20 minutes. The following premixed ingredients were then fed in at a steady rate over 5 hours:-

monomer premix (i)	42.944 parts
hydroxyisopropyl methacrylate	2.350 parts

Over the same 5-hour period, 3.672 parts of initiator solution (ii) was fed in separately at a constant rate. Thereafter the reaction mixture was kept at 80-85°C for 1 hour and then cooled to room temperature, giving a stable aqueous dispersion of crosslinked polymer micro-particles. The dispersion had a total solids content of 46.6% and a content of non-volatile solids insoluble in any organic solvent of 44.5%.

B. Preparation of basecoat composition

Premix (iv)

2.563 parts of the commercial thickener known as "Acrysol" ASE 60 ("Acrysol" is a Registered Trade Mark of Rohm & Haas Company) was stirred with sufficient of a 25% solution of dimethylaminoethanol in demineralised water to bring the pH to 7.65. Further demineralised water was then added to a total of 23.956 parts.

Premix (v)

A blend of 29.299 parts of the microparticle dispersion from stage A above and 18.614 parts of demineralised water was brought to a pH of 7.65 by addition of sufficient of a 25% solution of dimethylaminoethanol in demineralised water. There was then blended in 23.956 parts of premix (iv) prepared as described above.

T a stirred mixer were charged:-

aluminium paste (metal content, 65%) 5.133 parts

2-butoxyethanol 15.193 parts

The charge was stirred for 15 minutes, then the following

5 were added:-

hexamethoxymethyl melamine 3.696 parts

polypropylene glycol
(average mol.wt. 400) 2.464 parts

and stirring continued for a further 1 hour. Thereafter
there were added:-

10 premix (v) 71.869 parts

demineralised water 1.623 parts

and stirring continued for 1 hour more. The basecoat
composition thus obtained had the following character-
istics:-

15 solids content: 20.5%

apparent viscosity η_a : 34.6 poise at shear rate $D = 1 \text{ sec}^{-1}$
0.42 poise at $D = 10,000 \text{ sec}^{-1}$

C. Preparation of acrylic polymer for clearcoat composition

20 To a reactor fitted with stirrer, thermometer
and reflux condenser was charged 42.20 parts of isoprop-
anol. This was heated to reflux temperature (84°C) and the
following premixed ingredients were then added at a
steady rate over 3 hours:-

25 methyl methacrylate 19.85 parts

butyl acrylate 24.80 parts

hydroxyethyl methacrylate 2.48 parts

acrylic acid 2.48 parts

isopropanol 7.45 parts

30 benzoyl peroxide (60% paste
in dimethyl phthalate) 0.74 part

The reactants were maintained at reflux temperature for a further 2 hours. There was obtained a polymer solution of 50% solids content. From this there was removed, by direct distillation, 28.87 parts of isopropanol and to the residue there was added, with stirring, 1.86 parts of dimethylaminoethanol followed by 80.35 parts of demineralised water. Distillation of the azeotrope of isopropanol and water was then continued up to a temperature of 96-98°C, further demineralised water being added to replace the distillate. The total amount of distillate removed was 118.83 parts and the total amount of further demineralised water added was 114.65 parts. There was thus obtained an aqueous solution of acrylic polymer having a solids content of 33.5%.

15 D. Preparation of water-borne clearcoat composition

The following ingredients were blended together:-

	polymer solution from stage C above	75.16 parts
	hexamethoxymethylmelamine	6.29 parts
20	butoxyethanol	12.26 parts
	demineralised water	5.50 parts
	dimethylaminoethanol salt of p-toluenesulphonic acid (pH 7.6)	0.79 part

The clearcoat composition thus obtained had a solids content of 31.5% and a viscosity of 0.5 poise.

25 E. Application of basecoat and clearcoat to a substrate.

A metal panel was prepared with primer and surfacer, then three coats of the metallic basecoat composition described in stage B above were applied by spray, without further thinning, at a temperature of 25°C and a relative humidity of 51%. A one-minute flash-off period was allowed between the coats; the paint flow

rate at the spray gun was 400 mls/minute.

After the application of the third basecoat, the panel was dried at 35-42°C for 10 minutes and there were then applied three coats of the clearcoat composition described in stage D above. The three coats were applied wet-on-wet with a two-minute flash-off period between the coats and a final 3-minute flash-off period. The panel was then pre-heated at 70°C, followed by stoving at 150°C for 30 minutes.

The coating thus obtained had excellent 'flip' and freedom from shear and was equivalent in appearance to the best completely solvent-borne metallic paint system. Gloss and intercoat adhesion were good and there was no sinkage of the clearcoat into the basecoat.

15

EXAMPLE 4

A. Preparation of aqueous dispersion of polymer microparticles.

To a reactor fitted with stirrer, thermometer, reflux condenser and means for controlled introduction of two separate liquid feeds, was charged:-

demineralised water	29.030 parts
followed by a pre-mixed blend of	
methyl methacrylate	0.029 part
ammonium salt of sulphate of	
(nonylphenol + 5 mols.	
ethylene oxide)	0.029 part

The contents of the reactor were heated to 80-85°C with stirring and the following pre-mixed ingredients were added:-

butyl acrylate	0.069 part
methyl methacrylate	0.069 part

the reaction mixture was held at 80-85°C for 15 minutes, following which there was added a blend of:-

demineralised water	0.67 part
ammonium persulphate	0.021 part

After the contents of the reactor had been held at 80-85°C for a further 20 minutes, the following pre-mixed ingredients were fed into the reactor at a constant rate over 3 hours:-

butyl acrylate	10.758 parts
methyl methacrylate	10.189 parts
allyl methacrylate	0.686 part
ammonium salt of sulphate of (nonylphenol + 5 mols. ethylene oxide)	0.081 part

and simultaneously there was fed into the reactor at a steady rate, over the same period of 3 hours, a solution of 0.037 part of ammonium persulphate in 4.985 parts of demineralised water.

After completion of the above feeds, the contents of the reactor were held at 80-85°C for 1 hour. There was then added 34.716 parts of demineralised water and the temperature was brought back to 80-85°C; the following pre-mixed ingredients were then added at a constant rate over a period of 1 hour:-

methacrylic acid	0.950 part
butyl acrylate	2.035 parts
hydroxyethyl acrylate	1.357 parts
methyl methacrylate	0.950 part
ammonium salt of sulphate of (nonylphenol + 5 mols. ethylene oxide)	0.028 part

and simultaneously, at a steady rate over the same period of 1 hour, there was fed into the reactor a solution of 0.019 part of ammonium persulphate and 0.016 part of sodium borate in 0.596 part of demineralised water.

At the completion of both feeds, the temperature of the reaction mixture was held at 80-85°C for 1 hour, after which it was rapidly cooled to give a stable aqueous dispersion of polymer microparticles. The dispersion had a total non-volatile solids content of 30% and a content of non-volatile solids insoluble in organic solvents of 27%.

B. Preparation of basecoat composition

The dispersion obtained from stage A was brought to pH 8.0 by addition of dimethylaminoethanol, and 54.15 parts of this was charged to a mixer. There was then added, in the order stated, the following ingredients:-

	demineralised water	18.91 parts
	butoxyethanol	8.12 parts
	aluminium pigment concentrate (as described in Example 1(C))	18.02 parts

The mixture was stirred for 1 hour, to give a basecoat composition having the following characteristics:-

solids content: 25.8%

apparent viscosity η_a : 20 poise at shear rate $D = 1 \text{ sec}^{-1}$
0.2 poise at shear rate $D = 10,000 \text{ sec}^{-1}$

C. Application of basecoat and clearcoat to a substrate

To a metal panel prepared with primer and surfacer there were applied by spray, without further thinning, two coats of the metallic basecoat composition described in stage B above, at a temperature of 22°C and a relative humidity of 39%. The clearcoat composition subsequently applied was that described in stage F of Example 1, and the procedure for application of both

the basecoat and the clearcoat compositions was otherwise the same as that described in stage G of Example 1.

The results obtained were similar to those described in stage G of Example 1.

5

Comparative Example A

A. Preparation of silver metallic basecoat without microparticles.

To a stirred mixer were charged:-

	aluminium paste (metal content, 65%)	6.0 parts
10	2-butoxyethanol	18.7 parts

The charge was stirred for 30 minutes, then the following were added:-

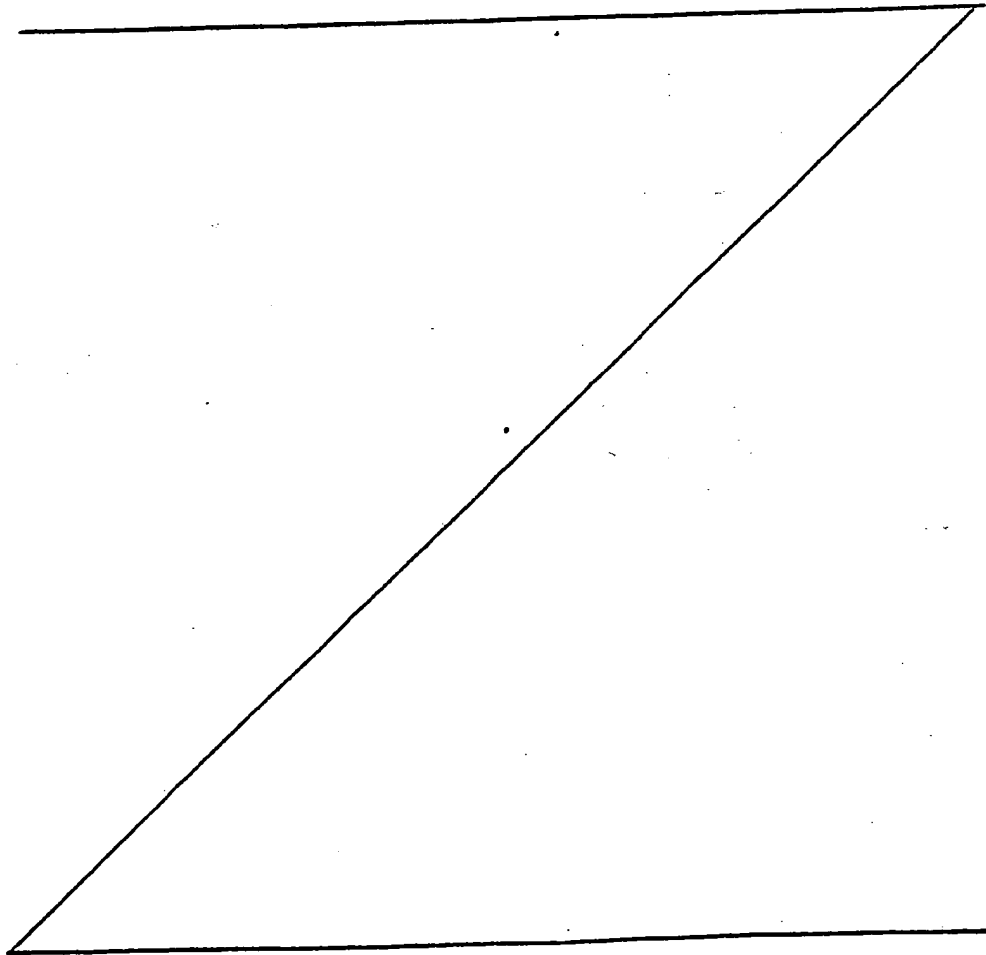
	hexamethoxymethylmelamine	4.3 parts
	polypropylene glycol (average mol.wt. 400)	2.9 parts

15 and stirring continued for a further 1 hour. There were then added, with stirring over a period of 30 minutes, 51.2 parts of a 33.5% solids aqueous solution of acrylic polymer made as described in Example 5(c) below, followed by addition of 16.9 parts of demineralised water.

20 A basecoat composition was thus obtained which had the same pigment:binder ratio, the same ratio of hexamethoxymethylmelamine to total non-volatile matter and a very similar value (0.3 poise) of the apparent viscosity η_a at $D = 10,000 \text{ sec}^{-1}$ as are quoted in
25 Example 1 for a basecoat composition according to the invention. The apparent viscosity at high shear rate of the composition containing no polymer microparticles indicated that it was suitable for application by spraying on to a substrate; but its apparent viscosity at low

shear rate, viz. $D = 1 \text{ sec}^{-1}$, was found to be approximately 1.0 poise only, showing that the composition had only slight pseudoplastic or thixotropic properties.

5 The basecoat composition was applied to a panel and overcoated with an acrylic clearcoat composition in the manner described in Example 1(G), the clearcoat composition employed being that described in Example 1(E) and (F). The silver metallic coating so obtained had a very poor 'flip' and exhibited patches of 'shear'. It was
10 also subject to 'popping' during the stoving operation.



Examples 1 - 4 illustrate the invention as applied to the production of "glamour metallic" finishes. In the following Example, its application to "solid colour" finishes is illustrated.

5

EXAMPLE 5

A. Preparation of white pigment millbase

The following ingredients were ground together in a ball mill for 16 hours:-

	Titanium dioxide pigment	31.3 parts
10	2-Butoxyethanol	18.9 parts
	Demineralised water	18.9 parts
	Dimethylaminoethanol	0.2 part
	Hexamethoxymethylmelamine	7.7 parts

The resulting millbase, which had a particle size of less than 0.5 micron, was then diluted with 11.6 parts of 2-butoxyethanol and 11.6 parts of demineralised water.

15

B. Preparation of blue pigment millbase

The following ingredients were ground together in a ball mill for 16 hours:-

20	Phthalocyanine blue pigment	12.9 parts
	2-Butoxyethanol	23.8 parts
	Demineralised water	23.8 parts
	Dimethylaminoethanol	0.2 part
	Hexamethoxymethylmelamine	9.7 parts

The resulting millbase, which had a particle size of less than 0.5 micron, was then diluted with 14.8 parts of 2-butoxyethanol and 14.8 parts of demineralised water.

25

C. Preparation of aqueous solution of acrylic polymer.

The following ingredients were blended:-

	Methyl methacrylate	19.9 parts
5	Butyl acrylate	24.8 parts
	Hydroxyethyl methacrylate	2.5 parts
	Acrylic acid	2.5 parts
	Isopropanol	7.4 parts
	Benzoyl peroxide	0.7 part

10 A mixture of 15.0 parts of the above blend and 42.2 parts of isopropanol was charged to a flask fitted with stirrer, thermometer, reflux condenser and means for adding a liquid feed at a controlled rate. The contents of the flask were heated to reflux temperature (84°C) and the remainder of

15 the above blend (42.8 parts) was added to them at a steady rate over a period of 3 hours. The reaction mixture was heated under reflux for a further 2 hours, to give a polymer solution of 51.0% solids content. To the solution there was then added 1.8 parts of dimethylaminoethanol,

20 the mixture was re-heated to reflux temperature and, with the condenser re-arranged, distillate was removed to a total of 33.0 parts while 85.0 parts of demineralised water were added, over a period of 10 hours. The finally resulting aqueous solution of acrylic polymer had a solids

25 content of 33.5%.

D. Preparation of blue basecoat composition

The following ingredients were mixed in the order stated:

	White millbase as described in (A), above	52.25 parts
	Blue millbase as described in (B), above	8.39 parts
5	Microparticle dispersion as described in Example 1(B)	14.62 parts
	Solution of acrylic polymer as described in (C) above	24.33 parts
	10% aqueous solution of p-toluene- sulphonic acid brought to pH 7.6 by addition of dimethylamino- ethanol	0.41 part

The resulting basecoat composition exhibited a viscosity
of 16.0 poise at a shear rate of 1 sec^{-1} and of 0.53
10 poise at a shear rate of $10,000 \text{ sec}^{-1}$.

E. Application of basecoat and clearcoat to a
substrate.

A metal panel was prepared with primer and surfacer, then
two coats of the blue basecoat composition described in (D)
15 above were applied by spray, without further thinning, at
a temperature of 22°C and a relative humidity of 39%. A
two-minute flash-off period was allowed between the coats.
After application of the second basecoat, the panel was
blown with air at 25°C and two coats of the clearcoat
20 composition as described in Example 1(F) were applied,
the clearcoat composition having been thinned beforehand
with xylene to a viscosity of 45 secs measured in a B.S.
B3 cup at 25°C . The two topcoats were applied wet-on-wet
with a two-minute flash-off between coats. After a final
25 three-minute flash-off, the panel was stoved at $125-130^{\circ}\text{C}$
for 30 minutes.

The resulting coating had good opacity and gloss and
there was no sinkage of the clearcoat into the basecoat.

Comparative Example B

A. Preparation of blue basecoat composition
without polymer microparticles.

The following ingredients were mixed in the order stated:-

	White millbase as described in Example 5(A)	54.8 parts
5	Blue millbase as described in Example 5(B)	8.8 parts
	Hexamethoxymethylmelamine	0.3 part
	Solution of acrylic polymer as described in Example 5(C)	35.7 parts
	10% aqueous solution of p-toluene- sulphonic acid, brought to pH 7.6 by addition of dimethylamino- ethanol	0.4 part

10 The resulting basecoat composition exhibited a viscosity
of 1.0 poise at a shear rate of 1 sec^{-1} and of 0.83 poise
at a shear rate of $10,000 \text{ sec}^{-1}$; that is to say, it poss-
essed very little pseudoplastic or thixotropic character.

B. Application of basecoat and clearcoat to a
substrate.

15 The procedure of Example 5(E) was repeated, but replacing
the basecoat composition described in Example 5(D) by the
basecoat described in (A) above. In this case, considerable
"popping" of the basecoat was observed, that is to say, air
entrained in the basecoat separated as bubbles, deforming
20 the surface of the film and damaging its smooth appearance.
Furthermore, a longer period than three minutes had to be
allowed between the application of the second basecoat and
that of the first clearcoat, otherwise the basecoat was
disturbed by the clearcoat with a deleterious effect upon
25 the final appearance of the panel.

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WE CLAIM :

1. A process for the production of a multi-layer protective and/or decorative coating upon a substrate surface, which comprises the steps of:-
 - (1) applying to the surface a basecoat composition comprising (a) a film-forming material, (b) a volatile liquid medium for the said material and (c) pigment particles dispersed in the said liquid medium;
 - (2) forming a polymer film upon the surface from the composition applied in step (1);
 - (3) applying to the basecoat film so obtained a transparent topcoat composition comprising (d) a film-forming polymer and (e) a volatile carrier liquid for the said polymer; and
 - (4) forming a second polymer film upon the basecoat film from the composition applied in step (3), characterised in that the constituents (a) and (b) of the basecoat composition are provided by a dispersion in an aqueous medium of crosslinked polymer microparticles which have a diameter in the range 0.01 to 10 microns, are insoluble in the said aqueous medium and are stable towards gross flocculation, the dispersion having a pseudoplastic or thixotropic character.
2. A process as claimed in claim 1, wherein the polymer microparticles are composed of acrylic addition polymers derived mainly from one or more alkyl esters of acrylic acid or methacrylic acid.
3. A process as claimed in claim 1 or claim 2, wherein the polymer microparticles are produced by a process of dispersion polymerisation of the constituent monomers in a medium which consists of water admixed with a volatile

organic co-solvent and which is as a whole capable of dissolving the monomers, the polymerisation being conducted at a temperature which is at least 10°C higher than the glass transition temperature of the polymer to be formed and in such a manner that at no time is there present a separate monomer phase, in the presence of a polymeric stabiliser having one component which is a polymer chain solvated by the aqueous medium and another component which is a polymer chain not solvated by that medium.

4. A process as claimed in claim 1 or claim 2, wherein the polymer microparticles are produced by aqueous emulsion polymerisation of the constituent monomers.
5. A process as claimed in claim 1 or claim 2, wherein the polymer microparticles are produced by a process of dispersion polymerisation of the constituent monomers in a non-aqueous medium in the presence of a steric stabiliser, followed by polymerisation in the dispersion thus obtained, also in the presence of a steric stabiliser, of one or more monomers which give rise to a second polymer which is inherently soluble in the aqueous medium of the basecoat composition at an appropriate pH, and finally by transfer of the resulting composite microparticles from the non-aqueous medium to the aqueous medium.
6. A process as claimed in any one of claims 1 to 5, wherein the basecoat composition contains a metallic pigment, has a solids content of less than 30% by weight non-volatiles, and has an apparent viscosity of less than 0.5 poise at a shear rate of $10,000 \text{ sec}^{-1}$ and of more than 20 poise at a shear rate of 1 sec^{-1} .
7. A process as claimed in any one of claims 1 to 5, wherein the basecoat composition contains a pigment

other than a metallic pigment, has a solids content of less than 30% by weight non-volatiles, and has an apparent viscosity of less than 1 poise at a shear rate of 10,000 secs^{-1} and of more than 5 poise at a shear rate of 1 sec^{-1} .

8. A process as claimed in claim 3 or claim 4, wherein the production of the polymer microparticles in aqueous medium is followed by further polymerisation in the same medium, in the presence of the microparticles, of monomers giving rise to an inherently water-soluble polymer.
9. A process as claimed in any one of claims 1 to 8, wherein a water-soluble polymer, capable of imparting pseudoplastic or thixotropic properties to the basecoat composition, has been added to the aqueous dispersion of the microparticles as a separate pre-formed ingredient.
10. A process as claimed in any one of claims 1 to 9, wherein the basecoat composition contains from 5% to 80% by weight of the polymer microparticles, based on the total non-volatile content of the composition.
11. A process as claimed in any one of claims 1 to 10, wherein the film-forming polymer constituent of the topcoat composition is an acrylic addition polymer derived mainly from one or more alkyl esters of acrylic acid or methacrylic acid.
12. A process as claimed in any one of claims 1 to 11, wherein, after application of the topcoat composition to the basecoat film, the coated substrate is subjected to a heating or curing operation.



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EUROPEAN SEARCH REPORT

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EP 81 30 1261

DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int. Cl.)
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	
	DE - A - 2 613 099 (DAI NIPPON TORYO) * Claims 1,2 * & GB - A - 1 517 834 --	1,6	B 05 D 7/26 5/06
PD	GB - A - 2 039 497 (ICI) * Page 1, line 105 - page 2, line 90; examples 24-27; claims 1-4 * --	1-5,7 8,10, 12	
A	FR - A - 2 388 865 (ICI) & GB - A - 1 588 976 (published 07-05-1981) --		B 05 D 7/26 7/16 5/06 C 09 D 5/38
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<input checked="" type="checkbox"/> The present search report has been drawn up for all claims			
Place of search The Hague		Date of completion of the search 30-06-1981	Examiner FRIDEN

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